



## **AVERAGE STRESS-STRAIN RELATIONSHIP OF STEEL BARS EMBEDDED IN CONCRETE**

**Shaohua CHEN<sup>1</sup> and Toshimi KABEYASAWA<sup>2</sup>**

### **SUMMARY**

In recent years, material property based modeling methods of reinforced concrete members are popularly adopted for nonlinear and dynamic frame analyses of structures, such as multi-spring model, fiber model and frame-element model for column and beam, also the panel model (macro-FEM) for shear wall. In these macro-models, concrete and steel bar are idealized as uniform and continuity materials, average stress-strain relations of concrete and steel bars should be used.

The average stress-strain relationships of concrete for reinforced concrete have been proposed in softening compression curve and stiffening tensile curve. By axial tension analysis of reinforced concrete bars with bond-slip relationship between steel bar and concrete, this study proposes an average stress-strain relationship of steel bars embedded in concrete. Also a bi-linear bond-slip model is proposed, the analytical approaches are stated. Using the average stress-strain relationship of steel bars for frame model of beam or column, a good correspondence between analytical and experimental results is obtained.

### **INTRODUCTION**

Many average stress-strain relation models of steel bar embedded in concrete are proposed based on experimental methods and analytical methods. In this paper, we propose an average stress-strain relation model by analytical methods with a bi-linear bond-slip model between steel bar and concrete. Using the proposed bi-linear bond-slip model, reinforced concrete bars under tension loading are analyzed and good correspondence is got. Based on statistical analysis of analytical results, the average stress-strain relation model is proposed. And we also proposed the relation in compression region considering the bulking of steel bar. Using the proposed stress-strain model, we did analysis for frame-element model for beam, good precision is got.

---

<sup>1</sup> Disaster Prevention Research Division, National Research Institute for Earth Science and Disaster Prevention, Tsukuba, Ibaraki, Japan

Email: sh\_chen@bosai.go.jp

<sup>2</sup> Earthquake Research Institute, The University of Tokyo, Tokyo, Japan

Email: kabe@eri.u-tokyo.ac.jp

## AVERAGE STRESS-STRAIN RELATION FOR CONCRETE

### Average Stress-strain Relation of Concrete

Without using hysteretic models based on force-displacement relations, material properties based macro-element models are popularly proposed in recent studies for reinforced concrete members. In our study, average stress-strain relation of concrete shown in Figure.1 is adopted.

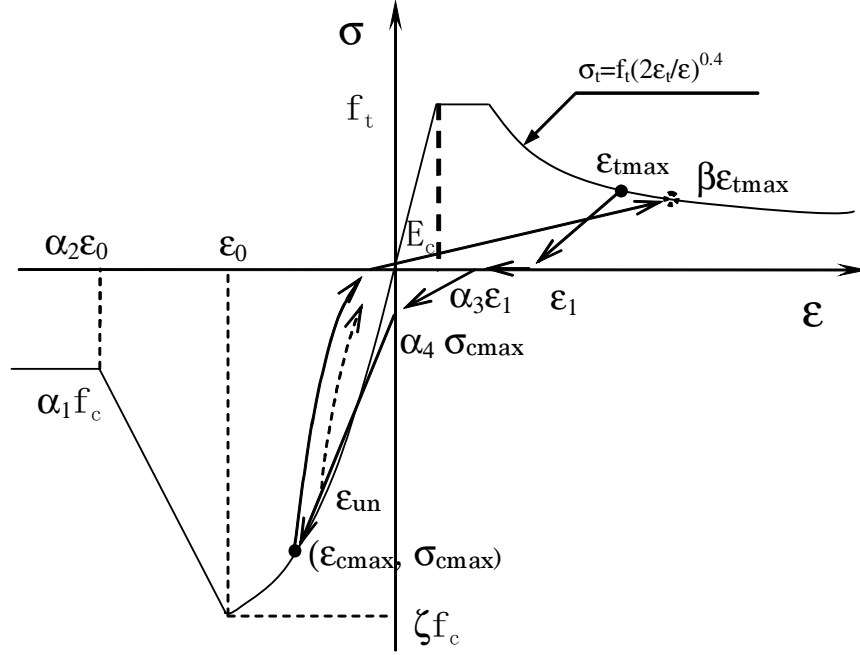


Figure.1: Average Stress-strain Relation of Concrete

Considering bond effect between steel bar and concrete, tension stiffening model is adopted for tension envelope [Izumo, Shima and Okamura, 1989]. But for plain concrete, tension strength is 0 after cracked like broken line. Under plane stress status for panel model of shear wall, stress softening model are adopted for compression envelope [Vecchio and Collins, 1982].

### Bond Stress-slip Relation between Steel Bar and Concrete

In order to analysis reinforced concrete bars under tension loading, a bi-linear model is proposed for bond stress-slip relation (Figure.1). The bond strength ( $\tau_u$ ) can be calculated with next formula (1) proposed by [Fujii and Morita, 1982],  $\tau_{c0}$  means the bond strength without stirrup bars,  $\tau_{st}$  stand for the effect of stirrup bars. But in yielding region of steel bar, the bond strength is reduced to  $0.2\tau_u$ .

$$\tau_u = \tau_{c0} + \tau_{st}$$

$$\tau_{c0} = (3.07b_i + 4.27) \cdot \sqrt{f_c}$$

$$\tau_{st} = 249kA_{st}/sND \cdot \sqrt{f_c}$$

(1)

Where,  $b_i$  is decided by splitting patterns shown in Figure.2 (a), (b) and (c), takes the minimum value of next  $b_{vi}$ ,  $b_{ci}$  and  $b_{si}$  calculated by formula (2).  $A_{st}$  stands for the sum of area of stirrup bars and  $s$  means the pitch of stirrup bars. The other parameters are shown in Figure.2.

$$\begin{aligned} b_{vi} &= \sqrt{3} \cdot (2c_{\min}/D + 1), \quad k = 0 \\ b_{ci} &= \sqrt{2} \cdot [(c_s + c_b)/D + 1] - 1, \quad k = \sqrt{2} \\ b_{si} &= b/ND - 1, \quad k = 1 \end{aligned} \quad (2)$$

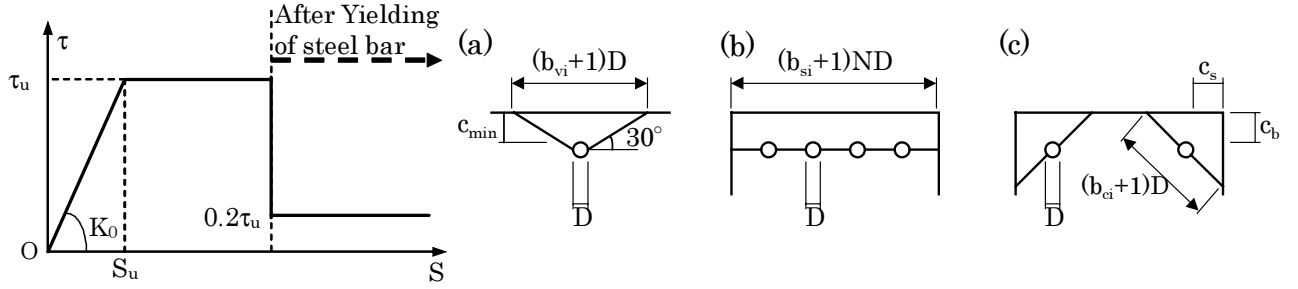


Figure.2: Bond Stress-slip Relation between Concrete and Steel Bar

The initial stiffness  $K_0$  can be shown as formula (3) [Iwata, Li and Ohno, 1998].

$$K_0 = 1160000 \times (f_c/2400)^{2/3} \times (13/D) \quad (KN/m^3) \quad (3)$$

Using the tension skeleton of concrete and bond-slip relation, the tension skeleton curve of steel bar is derived at next paragraph.

## THE AVERAGE STRESS-STRAIN RELATION FOR STEEL BAR

### Tension skeleton curve

The skeleton curve of bare bar is often simplified by O-A-B-C, but the skeleton curve of bar embedded in concrete can be simplified as a bi-linear model like O-A'-C' (Figure.3). Here,  $\epsilon_h = 0.015$ ,  $E_{sp} = 0.025E_s$ .

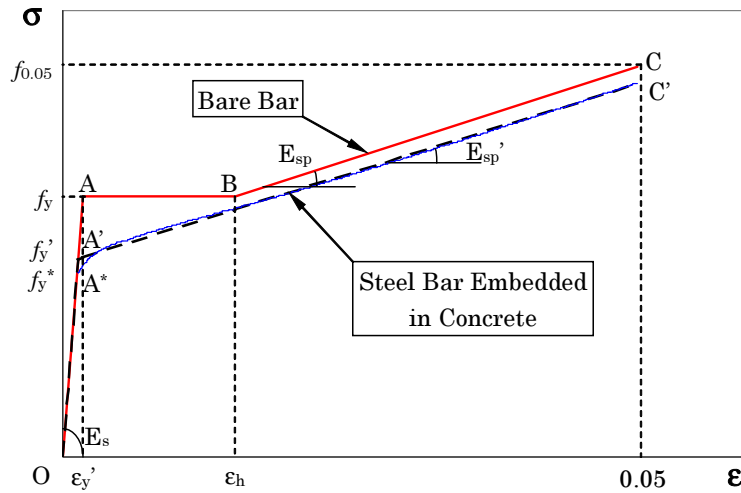


Figure.3: stress-strain relation of Steel Bar

The real yield strength of steel bar embedded in concrete can be calculated by next formula (4) [Hsu, 1993].

$$\frac{f_y^*}{f_y} = 1 - 1.5 \frac{\sqrt{n}}{\rho} \left( \frac{f_t}{f_y} \right)^{1.5} \quad (4)$$

Where,  $\rho$  stands for reinforcement ratio,  $n$  stands for rate of  $E_s/E_c$ .

In order to decide the look yield strength  $f_y'$  and harden stiffness  $E_{sp}$ , reinforced concrete bars will be analyzed under increment tension loading (Figure.4).

The distributions of stress and strain are shown as Figure.4. In the analysis, next suppositions are made.

- (1) Cracks have uniform distribution and same width.
- (2) Stress in concrete section has uniform distribution. As soon as the stress comes to the tension strength of concrete, crack occurs.
- (3) Concrete between cracks is elastic.
- (4) Stress and strain of concrete near crack are 0.
- (5) Bond stress distribution is symmetry between two close cracks.
- (6) There is no slip at the middle between two close cracks.

The slip between steel bar and concrete can be calculated by next formula (5).

$$S(x) = \int_0^x (\epsilon_s - \epsilon_c) dx \quad (5)$$

Balance of steel bar can be shown as formula (6) or (6').

$$\tau \cdot \pi D \cdot dx = E \cdot d\epsilon_s \cdot \pi D^2 / 4 \quad (6)$$

Or

$$\tau = C_s \frac{d\epsilon_s}{dx} \quad C_s = \begin{cases} E_s D/4 & \epsilon_s \leq \epsilon_y \\ E_{sp} D/4 & \epsilon_s > \epsilon_h \end{cases} \quad (6')$$

Balance of concrete can be represented by formula (7) or (7').

$$\tau \cdot \pi D \cdot dx = -E_c \cdot d\epsilon_c \cdot A_c \quad (7)$$

Or

$$\tau = -C_c \frac{d\epsilon_c}{dx} \quad C_c = E_c D/4 p_s \quad (7')$$

The boundary conditions can be shown as formula (8).

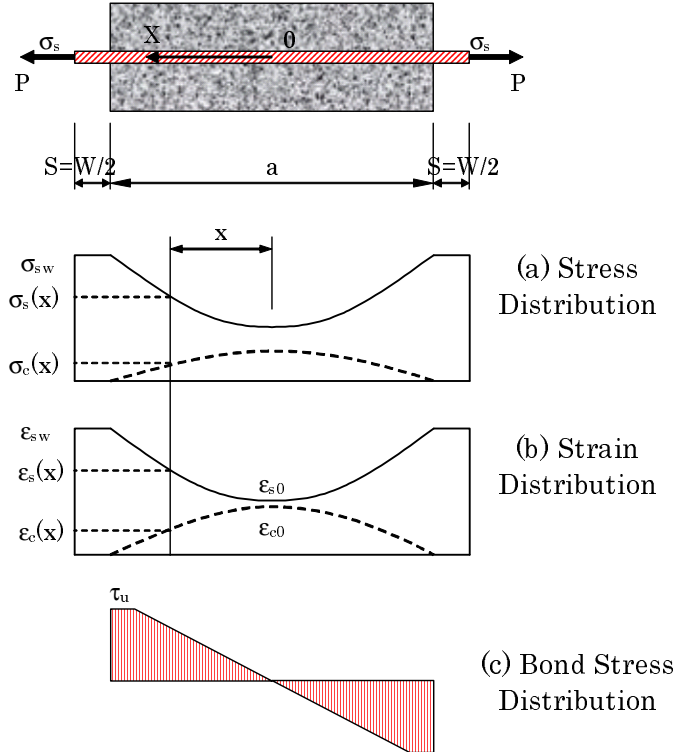


Figure.4 Bond Stress Distribution

$$\frac{d\varepsilon_s}{dx}\bigg|_{x=0} = 0, \quad \frac{d\varepsilon_c}{dx}\bigg|_{x=0} = 0, \quad \varepsilon_{c,x=\pm a/2} = 0 \quad (8)$$

Using above formula (5) – (8) and numerical method, average stress-strain relation of reinforced concrete bar can be solved. Figure.5 is a sample, the section is 125x125mm and the steel bar is deformed bar (D16). The analysis results (heavy line) reproduced experiment results (dotted line) with good precision; even the number of cracks had a good correspondence.

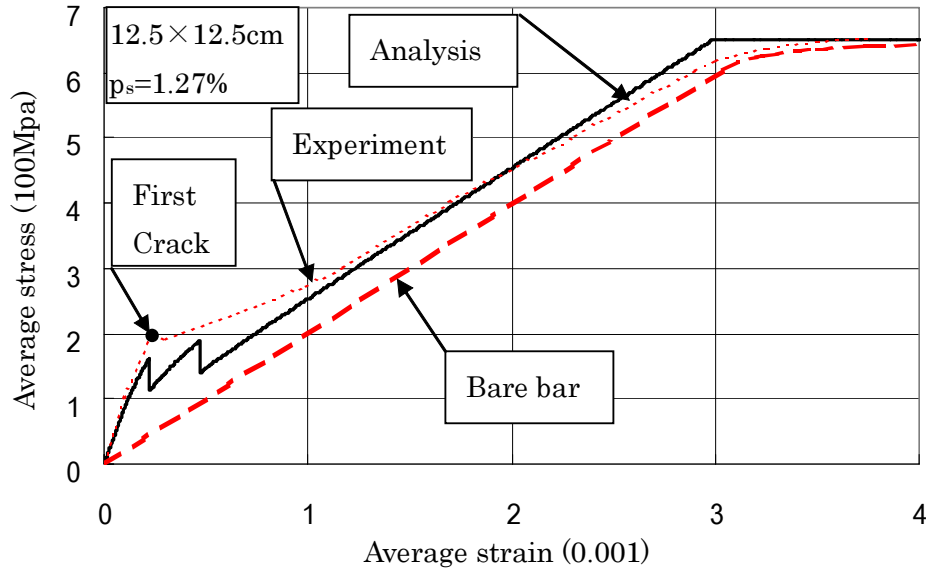


Figure.5 Average stress-strain relation of reinforced concrete bar

Cut out the tension contribution of concrete considered in tension stiffening model from the analysis results of reinforced concrete bar, average stress-strain relation of steel bar can be got. The left graph of Figure.6 shows the variation by parameter of reinforcement ratio  $p_s$ , and the right graph shows the variation by parameter of concrete strength  $f_c$ . In Figure.7, the influence of yield strength  $f_y$  of steel bar is shown.

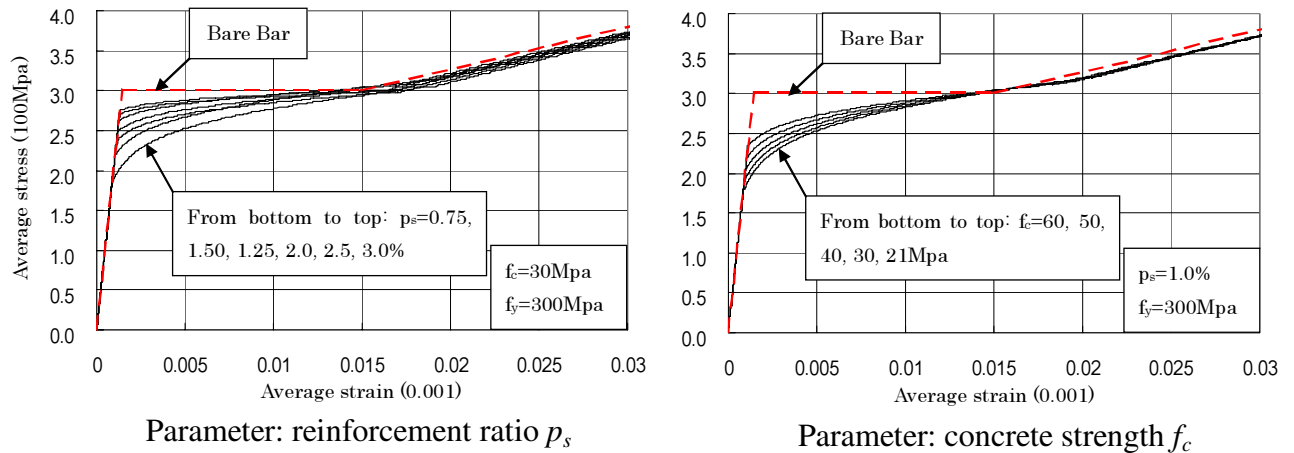


Figure.6 Average stress-strain relation of steel bar

Based on statistical analysis of analytical results with parameters of reinforcement ratio, concrete strength and steel yield strength, the look yield strength  $f_y^*$  and harden stiffness  $E_{sp}^*$  of bi-linear model can be shown as formula (9).

$$\begin{aligned} \frac{f_y^*}{f_y} &= 1 - 1.5 \frac{\sqrt{n}}{\rho} \left( \frac{f_t}{f_y} \right)^{1.5} \\ \frac{f_y^*}{f_y} &= 0.51 + 0.42 \frac{f_y^*}{f_y} \\ \frac{E_{sp}^*}{E_{sp}} &= 0.45 + 0.26 \frac{f_y}{100} + \left( 0.23 - 0.25 \frac{f_y}{100} \right) \cdot \left( \frac{f_y^*}{f_y} \right) \end{aligned} \quad (9)$$

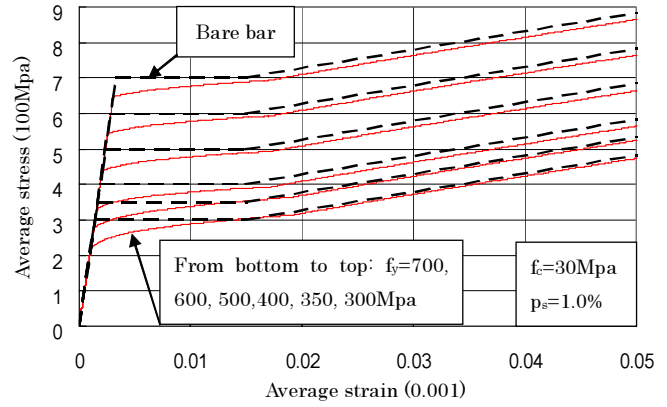


Figure.7 Average stress-strain relation of steel bar (Parameter: yield strength  $f_y$ )

### Compression skeleton curve

In compression region of steel bar, bond can be neglected, so the skeleton of steel bar embedded in concrete is same as bare bar. The yield strain of steel bar is about 0.002, the strain at concrete compressive strength is also around 0.002. Because of expansion and collapse of concrete loading over concrete strength, bulking of steel bar will occur, so the decrease of strength is considered after  $-1.5\epsilon_y$ . The inner rules are proposed like Figure.8.

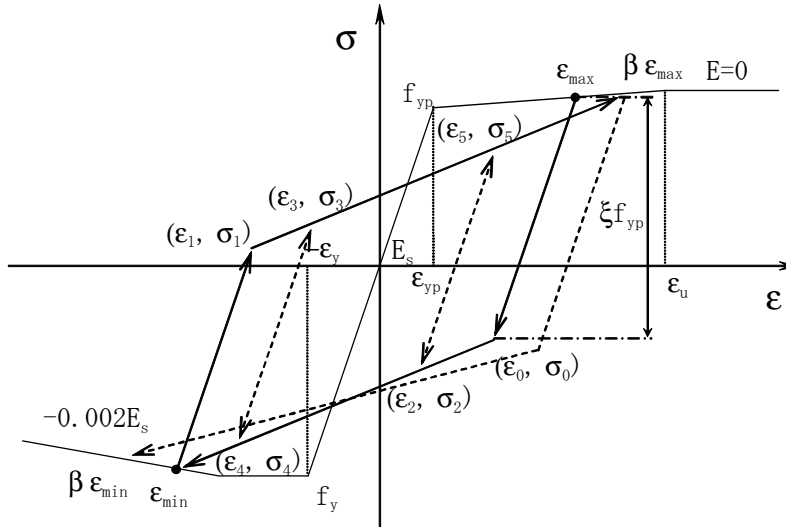


Figure.8 History model of steel bar

## THE ANALYSIS FOR REINFORCED CONCRETE MEMBER

### Experiment introduction

An experiment of cantilever is used to verify the proposed model, Figure.9 [Y. Kaneko, T. Kaneko and S. Otani, H. Shiohara, 2002]. In the experiment, only cyclic shear force is applied without axial force. The section of member is 200mm(width) x 300mm(height), and the shear span is 1150mm. The properties of concrete and steel bar are shown in Table.1.

Table.1 Properties of materials

Steel bar			
Type	Yield Strength [Mpa]	Tensile Strength [Mpa]	Modulus [Mpa]
D13	361	499	$186 \times 10^3$
$\phi 4$	478	509	$208 \times 10^3$
Concrete			
Age [Day]	Compressive Strength [Mpa]	Tensile Strength [Mpa]	Modulus [Mpa]
28	26.4	2.18	$30.4 \times 10^3$
54	27.4	2.49	$29.1 \times 10^3$
74	30.4	2.64	$27.2 \times 10^3$

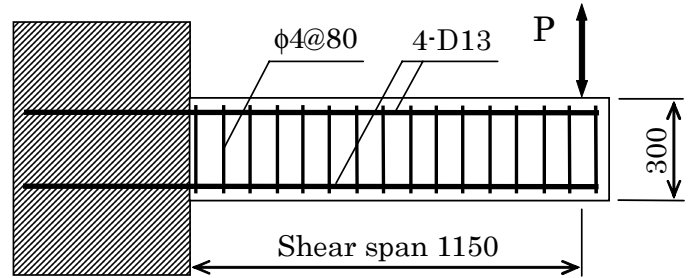


Figure.9 Sample of cantilever

### Analytical model

The cantilever is modeled by 3 frame-elements (Figure.10). Considering pull out of steel at fix end, length of the analytical model is 50mm longer than that of the member.

The section is divided into core concrete, cover concrete and steel bar. Core concrete has same properties of plain concrete without tension stiffening effect, cover concrete looks as reinforced concrete considering tension stiffening effect.

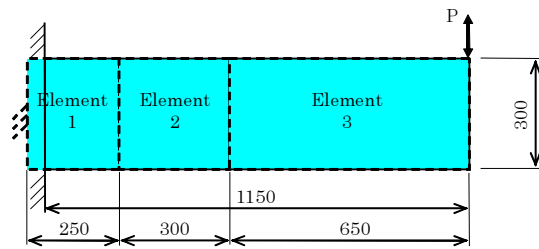


Figure.10 Analytical model of cantilever

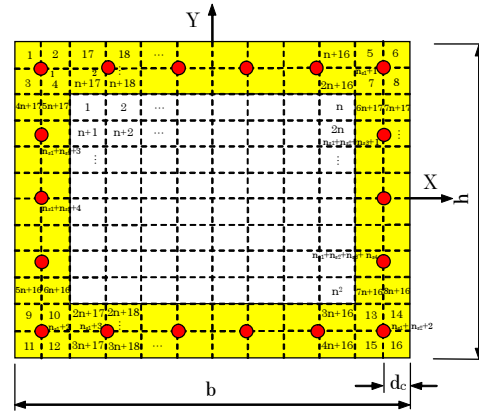


Figure.11 Cell division of section

### Results of analysis

The load-displacement relation of test is shown in Figure.12; the analytical result is shown in Figure.13. In testing, displacement is shifted to negative direction.

The relation between axial extension and displacement is shown in Figure.14. The axial extension means the strain of 200mm region at the fixed end.

Testing results are reproduced about initial stiffness, yield load and axial extension with good accuracy.

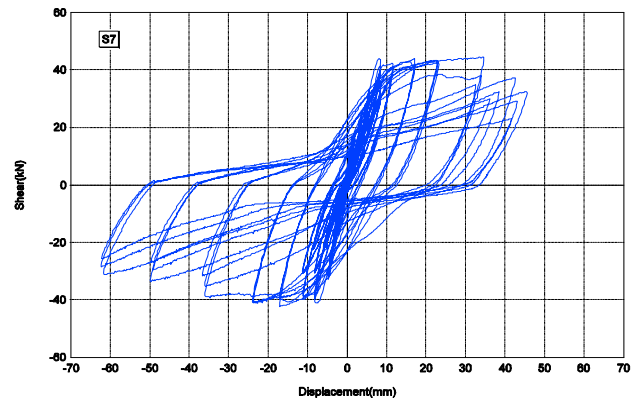


Figure.12 Load-displacement relation of test

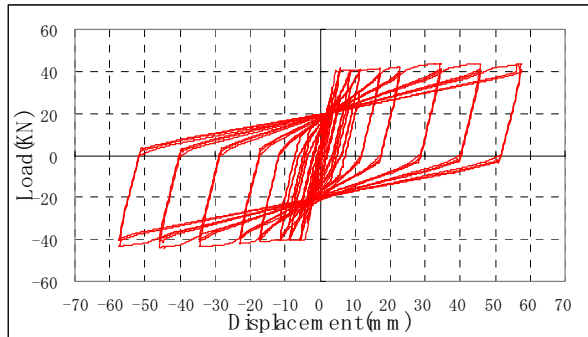


Figure.13 Load-displacement relation of analysis

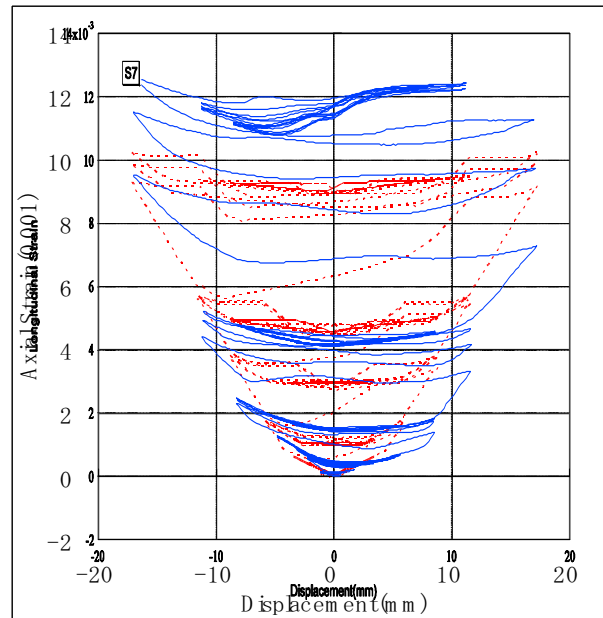


Figure.14 Axial extension to displacement

## RESULTS

The results of this paper can be concluded by next points.

1. Proposed a method to solve bond-slip problem for reinforced concrete bar under tension loading.
2. Proposed a bilinear model for steel bar embedded in concrete.
3. Analyzed a cantilever with the proposed model and good correspondence was got.

## REFERENCES

1. Hajime Okamura and Kohichi Maekawa, "Nonlinear Analysis and Constitutive Models of Reinforced Concrete", 1991
2. Vecchio, F.J. and Collins, M.P.: "Response of Reinforced Concrete to In-Plane Shear and Normal Stress", Department of Civil Engineering, Publication 82-03, University of Toronto, 1982.
3. Sakae Fujii and Shiro Morita, "Researches on Bond Strength of Deformed Steel Bar Part 1 Formula of Bond Strength", Journal of Structural and Construction Engineering, No.324, pp.24-22, February 1983
4. Tatsumi Iwata, Zhenbao Li and Yoshiteru Ohno, "Calculation of Long-term Deflections of Reinforced Concrete Slabs in Consideration of Steel Slippage at Fixed Edges", Journal of Structural and Construction Engineering, No.510, pp.145-152, August 1988
5. Hsu, T.T.C.: "Unified Theory of Reinforced Concrete", CRC Press, USA, 1993
6. Hiroshi Kaneko, Takashi Kaneko, Shunsuke Otani and Hitoshi Shiohara, "Influence of Shear Capacity and Loading-Rate Effect on Ductility of Reinforced Concrete Members", Summaries of Technical Papers of Annual Meeting Architectural Institute of Japan, Structure IV, C-2, pp.301-302, 2002